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## Development of Geological and Statistical Models for Forecasting the Confirmability of Structures in the Territory of the South of Perm Krai

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**Разработка геолого-статистических моделей для прогноза подтверждаемости структур на территории юга Пермского края**

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geological and morphological characteristics, amplitude of the structure, geological exploration, confirmability of structures by deep drilling, risk assessment, reflecting horizon, geological and statistical approach.

Today, 3D seismic surveys carried out in the south of Perm Krai are increasingly focused on identifying and preparing for deep drilling local geological structures, the amplitude of which is often comparable to the accuracy of structural constructions. Based on this, there is a need to develop a new geological and statistical approach that allows assessing the risks associated with the problem of unconfirmability of prepared objects by deep drilling. Minimizing such risks would reduce the number of negative results of exploration and appraisal drilling, which would directly affect the efficiency of the oil and gas producing enterprise in the field of geological exploration for oil and gas.

This article proposes one of the options for developing a geological-statistical approach to assessing the accuracy of the structural constructions of the studied area, which allows drawing conclusions about the degree of exploration of the territory under consideration. Based on the results obtained, conclusions were drawn about the correspondence of the structural plans of the reflecting horizons of the southern part of the Perm region with each other. A comparison of the obtained boundary values of discrepancies with the errors of structural constructions estimated from the results of 3D CDP seismic surveys in the south of Perm Krai.

This geological and statistical approach can be used to clarify the risks associated with the problem of unconfirmation of the geological and morphological characteristics of structures.

**Ключевые слова:**

геолого-морфологические характеристики, амплитуда структуры, геолого-разведочные работы, подтверждаемость структур глубоким бурением, оценка рисков, отражающий горизонт, геолого-статистический подход.

На сегодняшний день сейсморазведочные работы 3D, проводимые на территории юга Пермского края, все больше ориентированы на выявление и подготовку к глубокому бурению локальных геологических структур, амплитуда которых часто сопоставима с точностью структурных построений. Исходя из этого, возникает необходимость разработки нового геолого-статистического подхода, позволяющего оценить риски, связанные с проблемой неподтверждаемости подготовленных объектов глубоким бурением. Минимизация таких рисков позволила бы снизить количество отрицательных результатов поисково-оценочного бурения, что напрямую повлияло бы на эффективность деятельности нефтегазодобывающей предприятия в области геолого-разведочных работ на нефть и газ.

Предлагается один из вариантов разработки геолого-статистического подхода к оценке точности структурных построений изучаемой выборки, позволяющий сделать выводы о степени изученности рассматриваемой территории. На основе полученных результатов сделаны выводы о соответствии структурных планов отражающих горизонт южной части Пермского края между собой; также приводится сопоставление полученных граничных значений невязок с погрешностями структурных построений, оцененными по результатам выполнения сейсморазведочных работ МОИТ 3D в южной части Пермского края.

Данный геолого-статистический подход может применяться для уточнения рисков, связанных с проблемой неподтверждаемости геолого-морфологических характеристик структур.

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## Introduction

One of the ways to assess the accuracy of structural interpretations of reflecting horizons is considered in the paper, based on the analysis of the amplitude discrepancies between structures confirmed by drilling and structures prepared for deep drilling.

Minimizing the risks associated with the problem of prepared object unconfirmability by deep drilling would reduce the number of negative exploration and appraisal drilling, which would directly affect the efficiency of the oil and gas producing enterprise in the field of oil and gas geological exploration [1].

The studied sample comprised structures prepared for deep drilling by various methods (structural drilling, seismic exploration by the 2D and 3D common depth point (CDP) method). The sample size is sufficient to conduct a full-fledged regression analysis by reflecting horizons III (19 structures), II<sup>P</sup> (99 structures), II<sup>E</sup> (97 structures), I<sup>P</sup> (43 structures), I<sup>E</sup> (21 structures) [2–8].

To analyze the discrepancy nature between the amplitudes of structures according to drilling data ( $A_D$ ) and the amplitudes of structures prepared for deep drilling according to passport data ( $A_p$ ), and to assess the accuracy of structural constructions according to reflecting horizons III, II<sup>P</sup>, II<sup>E</sup>, I<sup>P</sup>, I<sup>E</sup>, a stepwise multiple regression was performed using Statistica software for groups with different numbers of structures  $N$ , already drilled at the time of the study in the southern region of the Perm Krai [9–24].

Independent variables in this study, in addition to the amplitude of the structure prepared for deep drilling, according to the data sheet ( $A_p$ ) were such geological and morphological characteristics as the length ( $D$ ) and width of the structure ( $S$ ), the width ratio of the structure to its length ( $S/D$ ), the area of the structure along the corresponding reflecting horizon ( $S_{RH}$ ), the intensity of the structure (I), the angle of consistency of the structure and the axis (or boundary) of the nearest tectonic element ( $\gamma$ ), the distance from the structure to the center ( $L^1_C$ ) and the nearest edge ( $L^1_E$ ) of the first-order tectonic element, the distance from the center of the first-order tectonic element ( $D^1_C$ ), calculated as the ratio of  $L^1_C$  to the sum of  $L^1_C$  and  $L^1_E$ , as well as the distance from the structure to the center ( $L^2_C$ ) and the nearest edge ( $L^2_E$ ) of a second-order tectonic element [25–42].

During the stepwise increase of  $N$ , the influence of statistically significant parameters on  $A_D$  was analyzed [43–52].

Bold font is used in tables to highlight statistically significant parameters, for which the  $p$ -criterion value, that characterizes the probability of a first-order errors type, is less than or equal to 0.05.

### Justification of the boundary values of the $|A_D - A_p|$ parameter for reflecting horizon III

Table 1 presents the results of the regression study  $A_D = f(A_p, S, D, S/D, S_{RH}, I, \gamma, L^1_C, L^1_E, D^1_C, L^2_C, L^2_E)$  with the  $|A_D - A_p|$  parameter in ascending order for reflecting horizon III.

As can be seen from the data in the table, regression was performed for  $N$  ranging from 9 to 19 structures inclusive, based on the reflecting horizon III.

The results of this regression study for reflecting horizon III allowed combining the obtained geo-statistical models, similar in the influence nature of significant parameters. Thus, for the reflecting horizon III, one class of structures was identified.

Statistically significant parameters controlling the model in the range of  $N$  from 9 to 19 are  $A_p$  and, fragmentarily  $S_{RH}$ , I,  $D^1_C$ .

The coefficient of multiple correlation ( $R^2$ ) in this interval varies from 0.523 to 1.000, gradually decreasing. The value of the  $p$ -criterion in the interval of the formed geo-statistical model fluctuates around 0.000–0.004.

Correlation field  $B = f(|A_D - A_p|)$  based on the results of regression analysis for reflecting horizon III is shown in Fig. 1, a.

When analyzing the data in Table 1 and Fig. 1, a, we see that there is no fundamental restructuring of the geo-statistical model in the considered interval  $|A_D - A_p|$  from 4 to 14 m, which suggests the existence of a boundary value of the  $|A_D - A_p|$  parameter outside the considered range.

### Justification of the boundary values of the $|A_D - A_p|$ parameter for the reflecting horizon II<sup>P</sup>

Table 2 presents the results of the regression study  $A_D = f(A_p, S, D, S/D, S_{RH}, I, \gamma, L^1_C, L^1_E, D^1_C, L^2_C, L^2_E)$  with the  $|A_D - A_p|$  parameter in ascending order based on the reflecting horizon II<sup>P</sup>.

Multiple correlation coefficient ( $R^2$ ) in this interval varies from 0.401 to 0.614, gradually decreasing. The  $p$ -criterion of the geo-statistical model formed in this interval fluctuates around 0.000.

Table 1

Results of the regression study  $A_D = f(A_p, S, D, S/D, S_{RH}, I, \gamma, L^1_C, L^1_E, D^1_C, L^2_C, L^2_E)$  with the  $|A_D - A_p|$  parameter in ascending order by reflecting horizon III

| No | $A_p$ ,<br>m | $A_D$ ,<br>m | $ A_D - A_p $ ,<br>m | $B$ , fr. of<br>units | Coefficients for parameters, fractions of units. |               |               |   |        |         |          |         |         |         | $R^2$ ,<br>fr. of<br>units | $p$ -cr.,<br>fr. of<br>units | $SE$ , m |  |
|----|--------------|--------------|----------------------|-----------------------|--|---------------|---------------|---|--------|---------|----------|---------|---------|---------|----------------------------|------------------------------|----------|--|
|    |              |              |                      |                       | $A_p$  | $S_{RH}$      | I             | D | S      | $S/D$   | $\gamma$ | $L^1_C$ | $L^1_E$ | $D^1_C$ | $L^2_C$                    | $L^2_E$                      |          |  |
| 1  | 6            | 6            | 0                    |                       |  |               |               |   |        |         |          |         |         |         |                            |                              |          |  |
| 2  | 14           | 14           | 0                    |                       |  |               |               |   |        |         |          |         |         |         |                            |                              |          |  |
| 3  | 21           | 21           | 0                    |                       |  |               |               |   |        |         |          |         |         |         |                            |                              |          |  |
| 4  | 6            | 7            | 1                    |                       |  |               |               |   |        |         |          |         |         |         |                            |                              |          |  |
| 5  | 7            | 8            | 1                    |                       |  |               |               |   |        |         |          |         |         |         |                            |                              |          |  |
| 6  | 9            | 7            | 2                    |                       |  |               |               |   |        |         |          |         |         |         |                            |                              |          |  |
| 7  | 12           | 14           | 2                    |                       |  |               |               |   |        |         |          |         |         |         |                            |                              |          |  |
| 8  | 9            | 6            | 3                    |                       |  |               |               |   |        |         |          |         |         |         |                            |                              |          |  |
| 9  | 7            | 3            | 4                    | -2.155                | 1.818  | -3.076        | -0.784        |   | -0.616 | 0.050   | -0.065   | 0.549   | -0.463  | 1.000   |                            | 0.000                        |          |  |
| 10 | 7            | 3            | 4                    | 0.782                 | <b>1.566</b>                                     | <b>-2.972</b> | <b>-0.953</b> |   |        | 0.149   | 0.063    | 0.030   | 0.993   | 0.002   | 0.797                      |                              |          |  |
| 11 | 9            | 13           | 4                    | -0.577                | <b>1.243</b>                                     | <b>-0.416</b> |               |   | 0.030  |         |          | 0.095   | 0.960   | 0.000   | 1.437                      |                              |          |  |
| 12 | 25           | 20           | 5                    | -0.577                | <b>1.243</b>                                     | <b>-0.416</b> |               |   | 0.030  |         |          | 0.095   | 0.960   | 0.000   | 1.437                      |                              |          |  |
| 13 | 9            | 3            | 6                    | 2.553                 | <b>0.828</b>                                     |               |               |   | -8.087 |         |          | 0.220   | 0.842   | 0.001   | 2.843                      |                              |          |  |
| 14 | 21           | 14           | 7                    | 5.095                 | <b>0.701</b>                                     |               |               |   | -7.260 |         |          | 0.237   | 0.810   | 0.001   | 3.014                      |                              |          |  |
| 15 | 17           | 9            | 8                    | 5.174                 | <b>0.687</b>                                     |               |               |   | -9.374 |         |          | 0.137   | 0.752   | 0.001   | 3.286                      |                              |          |  |
| 16 | 13           | 3            | 10                   | 3.518                 | <b>0.728</b>                                     |               |               |   | -8.259 |         |          | 0.136   | 0.638   | 0.001   | 3.703                      |                              |          |  |
| 17 | 14           | 3            | 11                   | 5.007                 | <b>0.651</b>                                     |               |               |   | -5.087 |         |          | 0.623   | 0.001   | 3.821   |                            |                              |          |  |
| 18 | 19           | 6            | 13                   | 6.913                 | <b>0.543</b>                                     |               |               |   |        | -9.016  |          | 0.529   | 0.004   | 4.236   |                            |                              |          |  |
| 19 | 22           | 8            | 14                   | 7.944                 | <b>0.505</b>                                     |               |               |   |        | -10.203 |          | 0.523   | 0.003   | 4.130   |                            |                              |          |  |

Table 2

Results of the regression study  $A_D = f(A_p, S, D, S/D, S_{RH}, I, \gamma, L^1_C, L^1_E, D^1_C, L^2_C, L^2_E)$   
with the  $|A_D - A_p|$  parameter in ascending order by the reflecting horizon II<sup>P</sup>

| No | $A_p$ ,<br>m | $A_D$ ,<br>m | $ A_D - A_p $ , m | B, fr. of<br>units | Coefficients for parameters, fractions of units. |              |              |              |              |              |              |         |         |         | $R^2$ , fr.<br>of<br>units | $p$ -cr.,<br>fr. of<br>units | $SE$ , m |       |
|----|--------------|--------------|-------------------|--------------------|--|--------------|--------------|--------------|--------------|--------------|--------------|---------|---------|---------|----------------------------|------------------------------|----------|-------|
|    |              |              |                   |                    | $A_p$  | $S_{RH}$     | $I$          | $D$          | $S$          | $S/D$        | $\gamma$     | $L^1_C$ | $L^1_E$ | $D^1_C$ | $L^2_C$                    | $L^2_E$                      |          |       |
| 1  | 6            | 6            | 0                 |                    |  |              |              |              |              |              |              |         |         |         |                            |                              | 1.000    | 0.000 |
| 2  | 12           | 12           | 0                 |                    |  |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.297 |
| 3  | 12           | 12           | 0                 |                    |  |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.328 |
| 4  | 14           | 14           | 0                 |                    |  |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.199 |
| 5  | 16           | 16           | 0                 |                    |  |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.327 |
| 6  | 18           | 18           | 0                 |                    |  |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.451 |
| 7  | 20           | 20           | 0                 |                    |  |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.325 |
| 8  | 20           | 20           | 0                 | 0.000              | 1.000  |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.126 |
| 9  | 8            | 7            | 1                 | <b>-2.016</b>      | <b>1.047</b>                                     | 0.035        | 0.290        |              | <b>0.014</b> |              |              |         |         |         |                            |                              |          | 0.998 |
| 10 | 13           | 12           | 1                 | 0.959              | <b>1.018</b>                                     |              |              | -1.857       | 0.010        |              |              |         |         |         |                            |                              |          | 0.998 |
| 11 | 13           | 12           | 1                 | <b>-3.789</b>      | <b>1.042</b>                                     |              |              | 1.154        | 0.007        | 0.050        | 0.040        |         |         |         |                            |                              |          | 0.998 |
| 12 | 14           | 13           | 1                 | <b>-3.306</b>      | <b>0.936</b>                                     | 0.525        | 0.076        |              | 0.010        | <b>0.055</b> | <b>0.038</b> |         |         |         |                            |                              |          | 0.219 |
| 13 | 15           | 14           | 1                 | <b>-3.380</b>      | <b>0.938</b>                                     | <b>0.536</b> | <b>0.080</b> |              | <b>0.010</b> | <b>0.054</b> | <b>0.037</b> |         |         |         |                            |                              |          | 0.199 |
| 14 | 20           | 19           | 1                 | <b>3.838</b>       | <b>1.064</b>                                     |              |              |              | 1.121        | <b>0.013</b> | <b>0.047</b> | 0.030   |         |         |                            |                              |          | 0.997 |
| 15 | 20           | 19           | 1                 | <b>-3.035</b>      | <b>0.995</b>                                     |              |              | 0.586        |              | <b>0.050</b> | <b>0.048</b> |         |         |         |                            |                              |          | 0.992 |
| 16 | 21           | 20           | 1                 | <b>-7.770</b>      | <b>1.077</b>                                     | -0.553       | -0.044       | 2.505        | -2.861       | <b>8.078</b> | <b>0.015</b> | 0.035   | 0.004   |         |                            |                              |          | 0.998 |
| 17 | 17           | 18           | 1                 | <b>-7.383</b>      | <b>1.117</b>                                     | -0.432       | -0.049       |              | 1.878        | 0.009        | 0.008        | 0.107   | 5.404   |         |                            |                              |          | 0.996 |
| 18 | 9            | 7            | 2                 | <b>-3.592</b>      | <b>1.083</b>                                     | -0.704       | -0.019       |              | <b>1.605</b> |              | 0.042        | 0.028   |         |         |                            |                              |          | 0.989 |
| 19 | 9            | 7            | 2                 | <b>-4.211</b>      | <b>1.166</b>                                     | -0.586       | -0.049       | 0.684        | 2.140        | 0.007        | 0.025        |         |         |         |                            |                              |          | 0.990 |
| 20 | 12           | 10           | 2                 | <b>-4.476</b>      | <b>1.167</b>                                     | -0.680       | -0.046       | 1.044        | 2.486        | 0.026        |              |         |         |         |                            |                              |          | 0.985 |
| 21 | 12           | 10           | 2                 | <b>-4.621</b>      | <b>1.211</b>                                     | -0.437       | -0.061       |              | <b>3.206</b> | 0.008        | 0.025        |         | -0.036  |         |                            |                              |          | 0.985 |
| 22 | 13           | 11           | 2                 | <b>-3.250</b>      | <b>1.066</b>                                     |              |              |              | 1.573        |              | 0.022        |         |         |         |                            |                              |          | 0.973 |
| 23 | 15           | 13           | 2                 | <b>-5.023</b>      | <b>1.213</b>                                     | -0.472       | -0.059       |              | <b>3.399</b> | 0.008        | 0.030        |         | -0.030  |         |                            |                              |          | 0.980 |
| 24 | 18           | 16           | 2                 | -1.584             | <b>1.061</b>                                     |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.949 |
| 25 | 27           | 25           | 2                 | -1.452             | <b>1.048</b>                                     |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.945 |
| 26 | 14           | 16           | 2                 | -0.925             | <b>1.008</b>                                     |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.953 |
| 27 | 24           | 26           | 2                 | -0.808             | <b>1.057</b>                                     |              | -0.377       |              |              |              |              |         |         |         |                            |                              |          | 0.955 |
| 28 | 34           | 36           | 2                 | -0.579             | <b>1.085</b>                                     |              |              |              |              |              |              |         | -1.641  | -0.036  |                            |                              |          | 0.973 |
| 29 | 13           | 10           | 3                 | -0.545             | <b>1.091</b>                                     |              |              |              |              |              |              |         | -1.790  | -0.045  |                            |                              |          | 0.972 |
| 30 | 14           | 11           | 3                 | -0.652             | <b>1.094</b>                                     |              |              |              |              |              |              |         | -1.914  | -0.039  |                            |                              |          | 0.968 |
| 31 | 15           | 12           | 3                 | -1.350             | <b>1.093</b>                                     |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.964 |
| 32 | 18           | 14           | 4                 | -0.810             | <b>1.067</b>                                     |              |              | 2.288        |              | -0.051       | -0.049       |         |         | -0.036  | 0.953                      | 0.000                        |          | 1.494 |
| 33 | 20           | 16           | 4                 | -1.661             | <b>1.049</b>                                     |              |              | 1.734        |              | -0.035       |              |         |         |         |                            |                              |          | 0.939 |
| 34 | 7            | 11           | 4                 | -0.026             | <b>1.033</b>                                     |              |              |              |              |              |              |         |         |         |                            |                              |          | 0.929 |
| 35 | 10           | 5            | 5                 | -2.032             | <b>1.053</b>                                     |              |              | 2.165        |              | -0.039       |              |         |         |         |                            |                              |          | 0.929 |
| 36 | 10           | 5            | 5                 | -2.736             | <b>1.064</b>                                     |              |              | 2.868        |              | -0.037       |              |         |         |         |                            |                              |          | 0.930 |
| 37 | 11           | 6            | 5                 | -1.838             | <b>1.070</b>                                     |              |              | 3.169        |              | -0.057       | -0.041       |         |         |         |                            |                              |          | 0.934 |
| 38 | 13           | 8            | 5                 | -1.202             | <b>1.083</b>                                     |              | 1.102        |              |              | -0.074       |              |         | -0.040  |         |                            |                              |          | 0.929 |
| 39 | 11           | 11           | 5                 | -0.896             | <b>1.076</b>                                     |              |              | 0.961        |              | -0.074       |              |         | -0.041  |         |                            |                              |          | 0.927 |
| 40 | 19           | 14           | 5                 | -1.202             | <b>1.083</b>                                     |              | 1.102        |              |              | -0.074       |              |         | -0.040  |         |                            |                              |          | 0.929 |
| 41 | 22           | 17           | 5                 | -0.896             | <b>1.076</b>                                     |              |              | 0.961        |              | -0.074       |              |         | -0.041  |         |                            |                              |          | 0.927 |
| 42 | 25           | 20           | 5                 | -0.802             | <b>1.057</b>                                     |              | 0.790        |              |              | -0.080       |              |         |         |         |                            |                              |          | 0.915 |
| 43 | 11           | 16           | 5                 | -2.412             | <b>1.039</b>                                     |              |              | 3.366        |              | -0.047       |              |         |         |         |                            |                              |          | 0.892 |
| 44 | 11           | 16           | 5                 | -1.876             | <b>1.019</b>                                     |              |              | 3.371        |              | -0.050       |              |         |         |         |                            |                              |          | 0.869 |
| 45 | 23           | 28           | 5                 | -4.665             | <b>1.013</b>                                     |              |              | <b>5.819</b> |              |              |              |         |         |         |                            |                              |          | 0.855 |
| 46 | 31           | 36           | 5                 | -5.479             | <b>1.060</b>                                     |              |              | <b>6.115</b> |              |              |              |         |         |         |                            |                              |          | 0.874 |
| 47 | 11           | 5            | 6                 | -5.757             | <b>1.074</b>                                     |              |              | <b>6.036</b> |              |              |              |         |         |         |                            |                              |          | 0.869 |
| 48 | 18           | 12           | 6                 | -3.539             | <b>1.074</b>                                     |              | -0.692       | 4.369        |              |              |              |         |         |         |                            |                              |          | 0.860 |
| 49 | 22           | 16           | 6                 | -5.097             | <b>1.046</b>                                     |              |              | <b>5.273</b> |              |              |              |         |         |         |                            |                              |          | 0.841 |
| 50 | 25           | 19           | 6                 | -4.271             | <b>1.040</b>                                     |              |              | -1.495       | <b>6.935</b> |              |              |         |         |         |                            |                              |          | 0.831 |
| 51 | 12           | 18           | 6                 | -4.178             | <b>1.012</b>                                     |              |              | -1.226       | <b>6.863</b> |              |              |         |         |         |                            |                              |          | 0.821 |
| 52 | 20           | 26           | 6                 | -2.751             | <b>1.006</b>                                     |              |              | <b>5.660</b> |              |              | -2.614       |         | -0.063  | 0.817   |                            |                              |          | 0.811 |
| 53 | 10           | 3            | 7                 | -3.015             | <b>1.030</b>                                     |              |              | <b>4.816</b> |              | -0.054       |              |         |         |         |                            |                              |          | 0.815 |
| 54 | 12           | 5            | 7                 | -2.545             | <b>1.037</b>                                     |              |              | 4.268        |              | -0.067       |              |         |         |         |                            |                              |          | 0.813 |
| 55 | 14           | 7            | 7                 | -3.454             | <b>1.047</b>                                     |              |              | 4.686        |              | -0.053       |              |         |         |         |                            |                              |          | 0.802 |
| 56 | 15           | 8            | 7                 | -3.357             | <b>1.044</b>                                     |              |              | <b>4.940</b> |              |              | -2.917       |         |         |         |                            |                              |          | 0.792 |
| 57 | 24           | 17           | 7                 | -1.848             | <b>1.015</b>                                     |              |              | 3.723        |              |              | -3.628       |         |         |         |                            |                              |          | 0.777 |
| 58 | 10           | 17           | 7                 | -2.921             | <b>1.006</b>                                     |              |              |              | 0.084        |              |              |         |         |         |                            |                              |          | 0.735 |
| 59 | 15           | 22           | 7                 | -2.502             | <b>1.003</b>                                     |              |              |              | 0.071        |              |              |         |         |         |                            |                              |          | 0.712 |
| 60 | 17           | 24           | 7                 | -2.497             | <b>0.951</b>                                     | 0.064        |              |              | 0.076        |              |              |         |         |         |                            |                              |          | 0.710 |
| 61 | 17           | 24           | 7                 | -2.693             | <b>0.961</b>                                     | 0.056        |              |              | 0.093        |              |              |         |         |         |                            |                              |          | 0.700 |
| 62 | 19           | 26           | 7                 | -3.050             | <b>1.019</b>                                     | 0.053        |              |              | <b>0.111</b> |              |              |         |         |         |                            |                              |          | 0.690 |
| 63 | 32           | 39           | 7                 | -3.764             | <b>1.072</b>                                     |              |              |              | 0.109        |              |              |         |         |         |                            |                              |          | 0.723 |
| 64 | 10           | 2            | 8                 | -5.178             | <b>1.089</b>                                     |              |              | 2.765        |              |              | 0.072        |         |         |         |                            |                              |          | 0.723 |
| 65 | 17           | 9            | 8                 | -5.041             | <b>1.077</b>                                     |              |              | 2.893        |              | 0.079        |              |         | -0.088  | 0.719   |                            |                              |          | 0.432 |
| 66 | 19           | 11           | 8                 | -5.390             | <b>1.068</b>                                     |              |              | 3.476        |              | 0.084        |              |         | -0.094  | 0.712   |                            |                              |          | 0.435 |
| 67 | 27           | 19           | 8                 | -2.519             | <b>1.075</b>                                     | -0.630       |              |              | 0.088        |              |              | -0.090  | 0.704   |         |                            |                              |          | 0.436 |
| 68 | 18           | 26           | 8                 | -2.760             | <b>1.084</b>                                     | -0.720       |              |              | 0.106        |              |              | -0.073  | 0.699   |         |                            |                              |          | 0.435 |
| 69 | 18           | 26           | 8                 | -3.030             | <b>1.086</b>                                     | -0.657       |              |              | <b>0.121</b> |              |              | -0.074  | 0.691   |         |                            |                              |          | 0.451 |
| 70 | 20           | 28           | 8                 | -2.686             | <b>1.104</b>                                     | -0.778       |              |              | 0.104        |              |              | -0.079  | 0.684   |         |                            |                              |          | 0.461 |
| 71 | 26           | 34           | 8                 | -2.233             | <b>1.120</b>                                     |              |              | -1.125       |              | 0.115        |              |         | -0.077  | 0.695   |                            |                              |          | 0.464 |
| 72 | 17           | 8            | 9                 | -2.676             | <b>1.116</b>                                     |              |              | -1.043       |              | 0.113        |              |         |         |         |                            |                              |          | 0.679 |
| 73 | 20           | 11           | 9                 | -2.848             | <b>1.105</b>                                     |              |              | -1.000       |              | <b>0.123</b> |              |         |         |         |                            |                              |          | 0.669 |
| 74 | 20           | 11           | 9                 | -2.463             | <b>1.102</b>                                     |              |              | -1.240       |              | <b>0.126</b> |              |         |         |         |                            |                              |          | 0.663 |
| 75 | 11           | 20           | 9                 | -4.086             | <b>1.052</b>                                     |              |              |              |              | <b>0.137</b> |              |         |         |         |                            |                              |          | 0.629 |
| 76 | 19           | 28           | 9                 | -3.818             | <b>1.062</b>                                     |              |              |              |              | <b>0.137</b> |              |         | -0.091  | 0.625   |                            |                              |          | 0.506 |
| 77 | 23           | 32           | 9                 | -4.219             | <b>1.077</b>                                     |              |              |              |              | <b>0.152</b> |              |         | -0.098  | 0.635   |                            |                              |          | 0.512 |
| 78 | 30           | 39           | 9                 | -4.846             | <b>1.109</b>                                     |              |              |              |              | <b>0.162</b> |              |         | -0.093  |         |                            |                              |          |       |

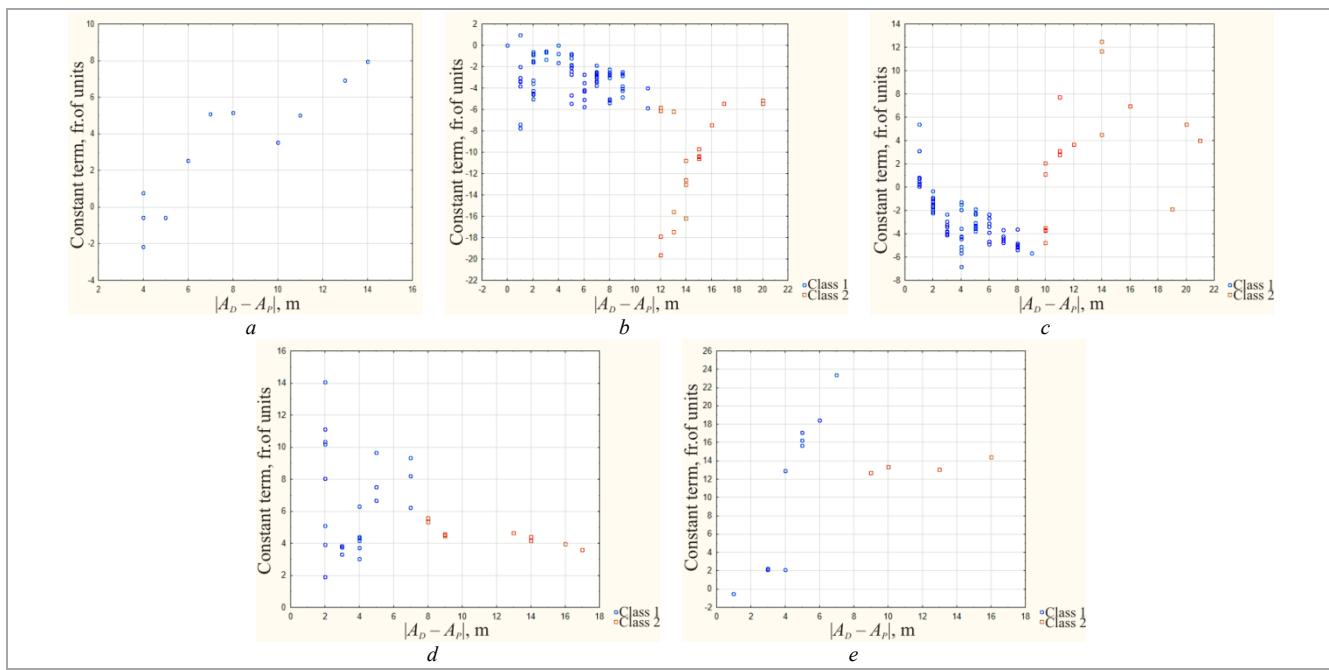


Fig. 1. Correlation field  $B = f(|A_D - A_p|)$  according to the results of regression analysis by reflecting horizon: *a* – III; *b* –  $\text{II}^P$ ; *c* –  $\text{II}^E$ ; *d* –  $\text{I}^P$ , *e* –  $\text{I}^E$

As can be seen from Table 2, the regression was performed for  $N$  from 8 to 99 structures inclusive along the  $\text{II}^P$  reflecting horizon.

The results of this regression analysis for reflecting horizon  $\text{II}^P$  allowed combining the obtained geo-statistical models, similar in the nature of the influence of significant parameters. Thus, two classes of structures were identified for the reflecting horizon  $\text{II}^P$ .

Class "1" corresponds to the first stable geo-statistical model, observed for  $N$  from 8 to 80.

Statistically significant parameters that control the model in this interval, are  $A_p$  and fragmentary,  $S$ ,  $D$ ,  $S/D$ ,  $S_{RH}$ ,  $I$ ,  $\gamma$ ,  $L^1_C$ ,  $L^1_E$ .

Multiple correlation coefficient ( $R^2$ ) in this interval varies from 0.620 to 1.000, gradually decreasing. The  $p$ -criterion in this interval of the formed geo-statistical model fluctuates around 0.000.

The reconstruction of the geo-statistical model from the first to the second occurs at  $N$  equal to 81.

Class "2" corresponds to the second stable geo-statistical model, observed at  $N$  from 81 to 99.

Statistically significant parameters that control the model in this interval are  $A_p$ ,  $S/D$ ,  $L^2_E$  and, fragmentarily,  $S$ ,  $D$ ,  $L^1_E$ ,  $L^2_E$ .

The correlation field  $B = f(|A_D - A_p|)$  based on the results of the regression analysis for the reflecting horizon  $\text{II}^P$  is presented in figure 1, *b*.

Having analyzed Table 2 and Fig. 1, *b*, we can conclude that the boundary value of the  $|A_D - A_p|$  parameter is in the range from 11 to 12 m (11.5 m is taken as the average value).

#### Justification of the boundary values of the $|A_D - A_p|$ parameter for the reflecting horizon $\text{II}^E$

Table 3 presents the results of the regression study  $A_D = f(A_p, S, D, S/D, S_{RH}, I, \gamma, L^1_C, L^1_E, D^1_C, L^2_C, L^2_E)$  with the  $|A_D - A_p|$  parameter in ascending order for the reflecting horizon  $\text{II}^E$ .

As can be seen from Table 3, the regression was performed for  $N$  from 8 to 97 structures inclusive for the reflecting horizon  $\text{II}^E$ .

The results of this regression study for reflecting horizon  $\text{II}^E$  allowed combining the obtained geo-

statistical models, similar in the nature of the influence of significant parameters. Thus, for the reflecting horizon  $\text{II}^E$  two classes of structures were identified.

Class "1" corresponds to the first stable geo-statistical model, observed at  $N$  from 11 to 80.

Statistically significant parameters that control the model in this interval are  $A_p$  and, in part,  $S$ ,  $S/D$ ,  $\gamma$ ,  $L^1_E$ ,  $D^1_C$ .

The multiple correlation coefficient ( $R^2$ ) in this interval varies between 0.667 and 1.000, gradually decreasing. The value of the  $p$ -criterion in this interval of the formed geo-statistical model fluctuates around 0.000.

The reconstruction of the geo-statistical model from the first to the second occurs at  $N$  equal to 81.

Class "2" corresponds to the second stable geological-statistical model, observed at  $N$  from 81 to 97.

Statistically significant parameters that control the model in this interval are  $A_p$ ,  $S_{RH}$  and, fragmentarily,  $L^1_E$ ,  $D^1_C$ .

The coefficient of multiple correlation ( $R^2$ ) in this interval varies from 0.408 to 0.673, gradually decreasing. The  $p$ -criterion in this interval of the formed geo-statistical model fluctuates around 0.000.

Correlation field  $B = f(|A_D - A_p|)$  based on the results of the regression analysis for reflecting horizon  $\text{II}^E$  is shown in Fig. 1, *c*.

Having analyzed the data in Table 3 and Fig. 1, *c*, we can conclude that the boundary value of the  $|A_D - A_p|$  parameter is in the range from 9 to 10 m (9.5 m is taken as the average value).

#### Justification of the boundary values of the $|A_D - A_p|$ parameter for the reflecting horizon $\text{I}^P$

Table 4 presents the results of the regression study  $A_D = f(A_p, S, D, S/D, S_{RH}, I, \gamma, L^1_C, L^1_E, D^1_C, L^2_C, L^2_E)$  with the  $|A_D - A_p|$  parameter in ascending order for the reflecting horizon  $\text{I}^P$ .

As can be seen from Table 4, the regression was performed for  $N$  from 10 to 43 structures inclusive for the reflecting horizon  $\text{I}^P$ .

The results of this regression study for reflecting horizon  $\text{I}^P$  allowed combining the obtained geo-statistical models, similar in the nature of the significant parameters influence. Thus, for the reflecting horizon  $\text{I}^P$  two classes of structures were identified.

Table 3

Results of the regression study  $A_D = f(A_p, S, D, S/D, S_{RH}, I, \gamma, L^1_C, L^1_E, D^1_C, L^2_C, L^2_E)$   
with the  $|A_D - A_p|$  parameter in ascending order by the reflecting horizon  $H^E$

| No | $A_p$ ,<br>m | $A_D$ ,<br>m | $ A_D - A_p $ ,<br>m | B, fr. of<br>units | Coefficients for parameters, fractions of units. |          |        |       |        |               |              |              |              |              | $R^2$ , fr.<br>of<br>units | $p-cr.$ ,<br>fr. of<br>units | $SE$ , m |       |       |       |       |  |
|----|--------------|--------------|----------------------|--------------------|--|----------|--------|-------|--------|---------------|--------------|--------------|--------------|--------------|----------------------------|------------------------------|----------|-------|-------|-------|-------|--|
|    |              |              |                      |                    | $A_p$  | $S_{RH}$ | $I$    | $D$   | $S$    | $S/D$         | $\gamma$     | $L^1_C$      | $L^1_E$      | $D^1_C$      | $L^2_C$                    | $L^2_E$                      |          |       |       |       |       |  |
| 1  | 7            | 7            | 0                    |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |
| 2  | 11           | 11           | 0                    |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |
| 3  | 12           | 12           | 0                    |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |
| 4  | 15           | 15           | 0                    |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |
| 5  | 18           | 18           | 0                    |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |
| 6  | 26           | 26           | 0                    |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |
| 7  | 6            | 5            | 1                    |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |
| 8  | 9            | 8            | 1                    |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |
| 9  | 10           | 9            | 1                    |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |
| 10 | 8            | 9            | 1                    |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |
| 11 | 9            | 10           | 1                    | 5.417              | 1.069  | 0.716    | -0.117 |       | -3.372 |               | -0.017       | 0.019        | 0.011        | -6.155       | 0.006                      | 0.098                        | 1.000    | 0.000 |       |       |       |  |
| 12 | 11           | 10           | 1                    | <b>3.096</b>       | <b>0.969</b>                                     |          |        |       |        | -4.067        | -0.024       | <b>0.059</b> | -2.455       | 0.075        | 0.029                      | 0.999                        | 0.000    | 0.317 |       |       |       |  |
| 13 | 11           | 10           | 1                    | 0.463              | <b>1.037</b>                                     |          |        |       |        | -3.233        | -0.007       | <b>0.053</b> |              |              |                            | 0.993                        | 0.000    | 0.577 |       |       |       |  |
| 14 | 12           | 11           | 1                    | 0.291              | <b>1.037</b>                                     |          |        |       |        | -3.139        | -0.007       | <b>0.057</b> |              |              |                            | 0.991                        | 0.000    | 0.594 |       |       |       |  |
| 15 | 11           | 12           | 1                    | 0.217              | <b>1.032</b>                                     |          |        |       |        | -2.966        | -0.010       | <b>0.067</b> |              |              |                            | 0.989                        | 0.000    | 0.619 |       |       |       |  |
| 16 | 13           | 12           | 1                    | 0.061              | <b>1.032</b>                                     |          |        |       |        | -2.916        | -0.008       | <b>0.068</b> |              |              |                            | 0.987                        | 0.000    | 0.643 |       |       |       |  |
| 17 | 14           | 13           | 1                    | 0.058              | <b>1.032</b>                                     |          |        |       |        | -2.881        | -0.008       | <b>0.067</b> |              |              |                            | 0.987                        | 0.000    | 0.616 |       |       |       |  |
| 18 | 15           | 14           | 1                    | 0.850              | <b>1.029</b>                                     |          |        |       |        | -3.610        | -0.014       | -0.014       | <b>0.076</b> |              |                            | 0.988                        | 0.000    | 0.609 |       |       |       |  |
| 19 | 25           | 26           | 1                    | 0.747              | <b>1.010</b>                                     |          |        |       |        | -2.999        | -0.018       | -0.015       | <b>0.069</b> |              | 0.050                      | -0.067                       | 0.994    | 0.000 | 0.565 |       |       |  |
| 20 | 9            | 7            | 2                    | -0.903             | <b>1.050</b>                                     |          |        |       |        | -1.844        |              |              | <b>0.056</b> |              |                            |                              | 0.984    | 0.000 | 0.758 |       |       |  |
| 21 | 8            | 10           | 2                    | -1.007             | <b>1.018</b>                                     |          |        |       |        |               | 0.032        |              |              |              |                            |                              | 0.971    | 0.000 | 0.978 |       |       |  |
| 22 | 12           | 10           | 2                    | -0.336             | <b>1.013</b>                                     |          |        |       |        | -2.360        |              | 0.049        |              | 0.037        |                            |                              | 0.973    | 0.000 | 0.980 |       |       |  |
| 23 | 12           | 10           | 2                    | -1.298             | <b>1.019</b>                                     |          |        |       |        |               | 0.042        |              |              |              |                            |                              | 0.965    | 0.000 | 1.025 |       |       |  |
| 24 | 15           | 13           | 2                    | -1.215             | <b>1.011</b>                                     |          |        |       |        |               | 0.038        |              |              |              |                            |                              | 0.960    | 0.000 | 1.076 |       |       |  |
| 25 | 17           | 19           | 2                    | -1.450             | <b>1.022</b>                                     |          |        |       |        |               | 0.038        |              |              | <b>0.048</b> |                            |                              |          | 0.958 | 0.000 | 1.109 |       |  |
| 26 | 17           | 19           | 2                    | -1.621             | <b>1.029</b>                                     |          |        |       |        |               | 0.038        |              |              | <b>0.055</b> |                            |                              |          | 0.958 | 0.000 | 1.119 |       |  |
| 27 | 17           | 19           | 2                    | -1.734             | <b>1.041</b>                                     |          |        |       |        |               | 0.038        |              |              | <b>0.057</b> |                            |                              |          | 0.956 | 0.000 | 1.160 |       |  |
| 28 | 26           | 28           | 2                    | -1.939             | <b>1.057</b>                                     |          |        |       |        |               | 0.038        |              |              | <b>0.058</b> |                            |                              |          | 0.965 | 0.000 | 1.150 |       |  |
| 29 | 27           | 29           | 2                    | -2.102             | <b>1.072</b>                                     |          |        |       |        |               | 0.038        |              |              | <b>0.058</b> |                            |                              |          | 0.971 | 0.000 | 1.144 |       |  |
| 30 | 33           | 35           | 2                    | -2.207             | <b>1.084</b>                                     |          |        |       |        |               | 0.038        |              |              | <b>0.056</b> |                            |                              |          | 0.979 | 0.000 | 1.129 |       |  |
| 31 | 9            | 6            | 3                    | -2.327             | <b>1.099</b>                                     |          |        |       |        |               | 0.045        |              |              |              |                            |                              |          | 0.975 | 0.000 | 1.242 |       |  |
| 32 | 3            | 6            | 3                    | -3.973             | <b>1.093</b>                                     |          |        |       |        | <b>2.889</b>  | 0.020        | 0.021        |              |              |                            |                              |          | 0.972 | 0.000 | 1.351 |       |  |
| 33 | 10           | 7            | 3                    | -4.124             | <b>1.097</b>                                     |          |        |       |        | <b>3.055</b>  | 0.017        | 0.021        |              |              |                            |                              |          | 0.968 | 0.000 | 1.434 |       |  |
| 34 | 11           | 8            | 3                    | -2.944             | <b>1.080</b>                                     |          |        |       |        | <b>3.074</b>  |              |              |              |              |                            |                              |          | 0.962 | 0.000 | 1.495 |       |  |
| 35 | 13           | 10           | 3                    | -3.225             | <b>1.071</b>                                     |          |        |       |        | 2.678         |              | 0.032        |              |              |                            |                              |          | 0.961 | 0.000 | 1.526 |       |  |
| 36 | 7            | 10           | 3                    | -3.361             | <b>1.058</b>                                     |          |        |       |        | <b>3.144</b>  |              | 0.039        |              |              |                            |                              |          | 0.959 | 0.000 | 1.551 |       |  |
| 37 | 14           | 11           | 3                    | -3.410             | <b>1.055</b>                                     |          |        |       |        | 2.863         |              | 0.049        |              |              |                            |                              |          | 0.956 | 0.000 | 1.579 |       |  |
| 38 | 15           | 12           | 3                    | -3.749             | <b>1.052</b>                                     |          |        |       |        | <b>3.508</b>  |              | 0.056        |              |              |                            |                              |          | 0.954 | 0.000 | 1.616 |       |  |
| 39 | 18           | 15           | 3                    | -3.833             | <b>1.046</b>                                     |          |        |       |        | <b>4.090</b>  |              | 0.041        |              |              |                            |                              |          | 0.945 | 0.000 | 1.687 |       |  |
| 40 | 10           | 6            | 4                    | -6.817             | <b>1.156</b>                                     |          | -0.186 | 1.910 | -5.269 | <b>12.408</b> |              | 0.044        |              |              |                            |                              |          | 0.951 | 0.000 | 1.702 |       |  |
| 41 | 12           | 8            | 4                    | -4.227             | <b>1.087</b>                                     |          | -0.099 |       |        | <b>4.707</b>  |              | 0.057        |              |              |                            |                              |          | 0.952 | 0.000 | 1.759 |       |  |
| 42 | 14           | 10           | 4                    | -4.446             | <b>1.087</b>                                     |          | -0.102 |       |        | <b>5.097</b>  |              | 0.059        |              |              |                            |                              |          | 0.965 | 0.943 | 0.000 | 1.763 |  |
| 43 | 16           | 12           | 4                    | -5.686             | <b>1.011</b>                                     | 0.619    |        |       |        | <b>5.129</b>  |              | <b>0.070</b> |              |              |                            |                              |          | 0.960 | 0.942 | 0.000 | 1.755 |  |
| 44 | 17           | 13           | 4                    | -5.409             | <b>0.999</b>                                     | 0.638    |        |       |        | <b>4.274</b>  |              | <b>0.079</b> |              |              |                            |                              |          | 0.950 | 0.933 | 0.000 | 1.857 |  |
| 45 | 10           | 14           | 4                    | -5.117             | <b>0.986</b>                                     | 0.681    |        |       |        | <b>4.273</b>  |              | <b>0.076</b> |              |              |                            |                              |          | 0.959 | 0.921 | 0.000 | 2.001 |  |
| 46 | 10           | 14           | 4                    | -1.271             | <b>0.981</b>                                     | 1.215    | -1.205 |       |        |               | <b>0.075</b> |              |              |              |                            |                              |          | 0.899 | 0.000 | 2.208 |       |  |
| 47 | 19           | 15           | 4                    | -1.508             | <b>0.966</b>                                     | 1.252    | -1.111 |       |        | <b>0.084</b>  |              |              |              |              |                            |                              | 0.895    | 0.000 | 2.219 |       |       |  |
| 48 | 13           | 17           | 4                    | -4.277             | <b>0.962</b>                                     | 0.698    |        |       |        | 3.310         |              | <b>0.086</b> |              |              |                            |                              |          | 0.896 | 0.000 | 2.218 |       |  |
| 49 | 13           | 17           | 4                    | -3.531             | <b>0.908</b>                                     | 0.993    | 0.101  |       |        |               | <b>0.107</b> |              | -0.054       | 0.884        | 0.000                      |                              |          | 0.884 | 0.000 | 2.323 |       |  |
| 50 | 15           | 19           | 4                    | -1.917             | <b>1.000</b>                                     |          |        |       |        |               | <b>0.101</b> |              |              |              |                            |                              |          | 0.860 | 0.876 | 0.000 | 2.348 |  |
| 51 | 8            | 3            | 5                    | -3.411             | <b>1.014</b>                                     |          |        |       |        | 2.551         |              | <b>0.090</b> |              |              |                            |                              |          | 0.068 | 0.879 | 0.000 | 2.371 |  |
| 52 | 12           | 7            | 5                    | -2.196             | <b>1.022</b>                                     |          |        |       |        |               | <b>0.078</b> |              |              |              |                            |                              |          | 0.856 | 0.000 | 2.529 |       |  |
| 53 | 13           | 8            | 5                    | -2.332             | <b>1.023</b>                                     |          |        |       |        |               | <b>0.081</b> |              |              |              |                            |                              |          | 0.850 | 0.000 | 2.570 |       |  |
| 54 | 14           | 9            | 5                    | -3.484             | <b>1.025</b>                                     |          |        |       |        | 2.495         |              | 0.059        |              |              |                            |                              |          | 0.846 | 0.000 | 2.613 |       |  |
| 55 | 17           | 12           | 5                    | -3.530             | <b>1.016</b>                                     |          |        |       |        | 2.530         |              | 0.064        |              |              |                            |                              |          | 0.840 | 0.000 | 2.642 |       |  |
| 56 | 11           | 16           | 5                    | -3.378             | <b>1.008</b>                                     |          |        |       |        | 2.770         |              | 0.059        |              |              |                            |                              |          | 0.825 | 0.000 | 2.738 |       |  |
| 57 | 12           | 17           | 5                    | -1.909             | <b>1.000</b>                                     |          |        |       |        |               | 0.077        |              |              |              |                            |                              |          | 0.805 | 0.000 | 2.845 |       |  |
| 58 | 14           | 19           | 5                    | -3.034             | <b>1.004</b>                                     |          |        |       |        | 2.664         |              | 0.057        |              |              |                            |                              |          | 0.801 | 0.000 | 2.900 |       |  |
| 59 | 16           | 21           | 5                    | -3.252             | <b>0.998</b>                                     |          |        |       |        | 2.297         |              | 0.046        |              | <b>0.070</b> |                            |                              |          | 0.799 | 0.000 | 2.951 |       |  |
| 60 | 26           | 31           | 5                    | -3.799             | <b>1.027</b>                                     |          |        |       |        | 2.784         |              | 0.047        |              | <b>0.065</b> |                            |                              |          | 0.817 | 0.000 | 2.975 |       |  |
| 61 | 13           | 7            | 6                    | -3.884             | <b>1.026</b>                                     |          |        |       |        | 2.510         |              | 0.051        |              | <b>0.071</b> |                            |                              |          | 0.809 | 0.000 | 3.032 |       |  |
| 62 | 22           | 16           | 6                    | -2.643             | <b>1.001</b>                                     |          |        |       |        |               | 0.079        |              | <b>0.069</b> |              | <b>0.794</b>               |                              |          | 0.794 | 0.000 | 3.101 |       |  |
| 63 | 11           | 17           | 6                    | -3.106             | <b>0.974</b>                                     | 0.412    |        |       |        |               | 0.080        |              | <b>0.082</b> |              |                            |                              |          | 0.780 | 0.000 | 3.207 |       |  |
| 64 | 15           | 21           | 6                    | -4.660             | <b>0.976</b>                                     | 1.596    |        |       |        | -3.590        | 6.222        |              | 0.060        | 0.091        |                            |                              |          | 0.784 | 0.000 | 3.243 |       |  |
| 65 | 18           | 24           | 6                    | -2.312             | <b>1.008</b>                                     |          |        |       |        | 3.352         | -0.020       |              |              | <b>0.059</b> |                            |                              |          | 0.764 | 0.000 | 3.364 |       |  |
| 66 | 19           | 25           | 6                    | -4.886             | <b>0.015</b>                                     | 1.445    |        |       |        | -3.230        | <b>7.691</b> |              |              | <b>0.084</b> |                            |                              |          | 0.775 | 0.000 | 3.357 |       |  |
| 67 | 20           | 26           | 6                    | -3.395             | <b>1.028</b>                                     | 0.364    |        |       |        |               | <b>4.939</b> | -0.020       |              |              |                            |                              |          | 0.771 | 0.000 | 3.410 |       |  |
| 68 | 10           | 3            | 7                    | -3.674             | <b>1.038</b>                                     | 0.418    |        |       |        |               | <b>4.864</b> | -0.021       |              |              |                            |                              |          | 0.767 | 0.000 | 3.473 |       |  |
| 69 | 13           | 6            | 7</td                |                    |  |          |        |       |        |               |              |              |              |              |                            |                              |          |       |       |       |       |  |

Table 4

Results of the regression study  $A_D = f(A_p, S, D, S/D, S_{RH}, I, \gamma, L^1_C, L^1_E, D^1_C, L^2_C, L^2_E)$   
with the  $|A_D - A_p|$  parameter in ascending order by the reflecting horizon  $I^P$

| No | $A_p$ ,<br>m | $A_D$ ,<br>m | $ A_D - A_p $ ,<br>m | B, fr. of<br>units | Coefficients for parameters, fractions of units. |               |               |        |        |              |          |              |         |         | $R^2$ ,<br>fr. of<br>units | $p$ -cr.,<br>fr. of<br>units | $SE$ , m |       |       |
|----|--------------|--------------|----------------------|--------------------|--|---------------|---------------|--------|--------|--------------|----------|--------------|---------|---------|----------------------------|------------------------------|----------|-------|-------|
|    |              |              |                      |                    | $A_p$  | $S_{RH}$      | $I$           | $D$    | $S$    | $S/D$        | $\gamma$ | $L^1_C$      | $L^1_E$ | $D^1_C$ | $L^2_C$                    | $L^2_E$                      |          |       |       |
| 1  | 7            | 7            | 0                    |                    |  |               |               |        |        |              |          |              |         |         |                            |                              |          |       |       |
| 2  | 7            | 7            | 0                    |                    |  |               |               |        |        |              |          |              |         |         |                            |                              |          |       |       |
| 3  | 9            | 9            | 0                    |                    |  |               |               |        |        |              |          |              |         |         |                            |                              |          |       |       |
| 4  | 3            | 2            | 1                    |                    |  |               |               |        |        |              |          |              |         |         |                            |                              |          |       |       |
| 5  | 3            | 4            | 1                    |                    |  |               |               |        |        |              |          |              |         |         |                            |                              |          |       |       |
| 6  | 6            | 5            | 1                    |                    |  |               |               |        |        |              |          |              |         |         |                            |                              |          |       |       |
| 7  | 6            | 7            | 1                    |                    |  |               |               |        |        |              |          |              |         |         |                            |                              |          |       |       |
| 8  | 7            | 8            | 1                    |                    |  |               |               |        |        |              |          |              |         |         |                            |                              |          |       |       |
| 9  | 9            | 8            | 1                    |                    |  |               |               |        |        |              |          |              |         |         |                            |                              |          |       |       |
| 10 | 2            | 4            | 2                    | 8.029              | 0.554  |               | -0.210        | -0.029 | -1.919 |              | -0.034   | -0.043       | -0.015  |         | -0.022                     | -0.080                       | 1.000    | 0.000 |       |
| 11 | 6            | 4            | 2                    | <b>14.061</b>      |  |               |               |        |        | -10.577      |          | -0.030       |         |         | -0.205                     | -0.175                       | 0.935    | 0.001 | 0.729 |
| 12 | 6            | 4            | 2                    | <b>10.198</b>      |  |               |               | 0.861  |        | -6.770       |          | -0.021       |         |         | -0.201                     |                              | 0.900    | 0.001 | 0.862 |
| 13 | 7            | 5            | 2                    | 10.352             |  |               | -0.282        | 1.500  | -3.265 | -1.207       | -0.035   | -0.025       |         |         | -0.073                     |                              | 0.943    | 0.008 | 0.774 |
| 14 | 6            | 8            | 2                    | <b>11.119</b>      |  |               | <b>-0.400</b> | 1.305  | -3.667 | -0.332       | -0.048   | -0.028       |         |         |                            |                              | 0.938    | 0.001 | 0.713 |
| 15 | 11           | 9            | 2                    | 1.904              | <b>0.727</b>                                     |               |               |        |        | -0.017       |          |              |         |         |                            | 0.090                        | 0.774    | 0.001 | 1.173 |
| 16 | 10           | 12           | 2                    | <b>5.089</b>       | <b>0.592</b>                                     |               |               |        |        | -5.559       |          | 0.033        |         |         |                            |                              | 0.782    | 0.000 | 1.348 |
| 17 | 15           | 13           | 2                    | <b>3.930</b>       | <b>0.695</b>                                     |               |               |        |        | -4.647       |          | 0.034        |         |         |                            |                              | 0.836    | 0.000 | 1.329 |
| 18 | 7            | 4            | 3                    | 3.329              | <b>0.693</b>                                     |               |               |        |        | -4.146       |          | 0.044        |         |         |                            |                              | 0.785    | 0.000 | 1.507 |
| 19 | 8            | 5            | 3                    | <b>3.757</b>       | <b>0.668</b>                                     |               |               |        |        | -4.837       |          | 0.047        |         |         |                            |                              | 0.777    | 0.000 | 1.496 |
| 20 | 8            | 5            | 3                    | <b>3.765</b>       | <b>0.645</b>                                     |               |               |        |        | -4.975       |          | 0.055        |         |         |                            |                              | 0.755    | 0.000 | 1.532 |
| 21 | 9            | 6            | 3                    | <b>3.831</b>       | <b>0.615</b>                                     |               |               |        |        | -5.113       |          | 0.064        |         |         |                            |                              | 0.742    | 0.000 | 1.526 |
| 22 | 7            | 3            | 4                    | <b>4.306</b>       | <b>0.614</b>                                     |               |               |        |        | -5.906       |          | 0.056        |         |         |                            |                              | 0.721    | 0.000 | 1.599 |
| 23 | 7            | 3            | 4                    | <b>4.149</b>       | <b>0.608</b>                                     |               |               |        |        | -5.996       |          | 0.063        |         |         |                            |                              | 0.688    | 0.000 | 1.696 |
| 24 | 7            | 3            | 4                    | <b>3.707</b>       | <b>0.626</b>                                     |               | -0.054        |        |        | -5.122       |          | <b>0.081</b> |         |         |                            |                              | 0.746    | 0.000 | 1.574 |
| 25 | 8            | 4            | 4                    | <b>4.406</b>       | <b>0.584</b>                                     |               |               |        |        | -6.471       |          | <b>0.070</b> |         |         |                            |                              | 0.694    | 0.000 | 1.660 |
| 26 | 4            | 8            | 4                    | 3.018              | <b>0.644</b>                                     |               | -0.121        | 1.154  | -3.786 |              | -0.001   | <b>0.102</b> |         | -0.089  | 0.154                      | 0.768                        | 0.000    | 1.624 |       |
| 27 | 7            | 11           | 4                    | <b>6.310</b>       | <b>0.683</b>                                     |               | -0.134        |        | -2.875 | -2.830       |          | 0.087        |         | -0.122  | 0.208                      | 0.679                        | 0.001    | 1.912 |       |
| 28 | 12           | 7            | 5                    | <b>6.686</b>       | <b>0.606</b>                                     | <b>-1.024</b> | -0.112        |        |        | -5.146       |          | 0.086        |         | -0.108  | 0.196                      | 0.648                        | 0.002    | 1.955 |       |
| 29 | 3            | 8            | 5                    | <b>7.534</b>       | <b>0.544</b>                                     | -0.134        |               |        | -3.364 | -3.145       |          | <b>0.108</b> |         | -0.118  | 0.166                      | 0.615                        | 0.002    | 2.009 |       |
| 30 | 15           | 20           | 5                    | <b>9.653</b>       | <b>0.786</b>                                     | -0.173        |               |        | -4.282 |              |          | -4.340       |         | -0.116  | 0.248                      | 0.685                        | 0.000    | 2.343 |       |
| 31 | 10           | 3            | 7                    | <b>8.186</b>       | <b>0.560</b>                                     | -0.106        | 1.444         |        | -4.950 |              |          | -5.434       |         | 0.031   |                            | 0.641                        | 0.000    | 2.492 |       |
| 32 | 2            | 9            | 7                    | <b>9.341</b>       | 0.466  | -0.113        | 1.630         |        | -5.249 |              |          | -6.044       |         | 0.029   |                            | 0.623                        | 0.000    | 2.517 |       |
| 33 | 11           | 18           | 7                    | 6.240              | 0.463  |               |               |        |        | -10.323      | 0.026    | 0.124        |         | 0.062   |                            | 0.525                        | 0.001    | 3.094 |       |
| 34 | 1            | 9            | 8                    | <b>5.325</b>       |  | <b>2.577</b>  |               |        |        | 0.020        |          | -5.811       |         |         |                            | 0.415                        | 0.001    | 3.266 |       |
| 35 | 6            | 14           | 8                    | <b>5.594</b>       |  | <b>2.577</b>  |               |        |        | 0.020        |          | -5.811       |         |         |                            | 0.415                        | 0.001    | 3.266 |       |
| 36 | 10           | 1            | 9                    | <b>4.558</b>       |  | <b>2.828</b>  |               |        |        | 0.022        |          | -5.399       |         |         |                            | 0.407                        | 0.001    | 3.422 |       |
| 37 | 14           | 5            | 9                    | <b>4.430</b>       |  | <b>2.824</b>  |               |        |        | 0.023        |          | -5.331       |         |         |                            | 0.405                        | 0.001    | 3.387 |       |
| 38 | 15           | 6            | 9                    | <b>4.529</b>       |  | <b>2.817</b>  |               |        |        | 0.022        |          | -5.468       |         |         |                            | 0.404                        | 0.000    | 3.344 |       |
| 39 | 22           | 9            | 13                   | <b>4.651</b>       |  | <b>2.777</b>  |               |        |        | 0.022        |          | -5.568       |         |         |                            | 0.407                        | 0.000    | 3.298 |       |
| 40 | 3            | 3            | 14                   | <b>4.419</b>       |  | <b>2.831</b>  |               |        |        | 0.023        |          | -5.459       |         |         |                            | 0.418                        | 0.000    | 3.262 |       |
| 41 | 3            | 17           | 14                   | <b>4.154</b>       |  | <b>2.510</b>  |               |        |        | <b>0.039</b> |          | -4.380       |         |         |                            | 0.352                        | 0.003    | 3.689 |       |
| 42 | 8            | 24           | 16                   | 3.943              |  | <b>2.420</b>  |               |        |        | <b>0.047</b> |          | -3.460       |         |         |                            | 0.245                        | 0.013    | 4.523 |       |
| 43 | 18           | 1            | 17                   | 3.614              |  | <b>2.362</b>  |               |        |        | <b>0.051</b> |          | -3.182       |         |         |                            | 0.240                        | 0.013    | 4.574 |       |

Class "1" corresponds to the first stable geo-statistical model, observed for  $N$  from 10 to 33.

Statistically significant parameters that control the model in this interval are  $A_p$  and, fragmentarily,  $S$ ,  $S/D$ ,  $S_{RH}$ ,  $I$ ,  $\gamma$ ,  $L^1_E$ ,  $D^1_C$ ,  $L^2_C$ .

Multiple correlation coefficient ( $R^2$ ) in this interval varies from 0.525 to 1.000, gradually decreasing. The value of the  $p$ -criterion in this interval of the formed geo-statistical model fluctuates around 0.000–0.008.

The reconstruction of the geo-statistical model from the first to the second occurs at  $N$  equal to 34.

Class "2" corresponds to the second stable geo-statistical model, observed at  $N$  from 34 to 43.

Statistically significant parameters controlling the model in this interval are  $D$  and fragmentarily  $\gamma$ ,  $D^1_C$ . The coefficient of multiple correlation ( $R^2$ ) in this interval varies from 0.240 to 0.418, gradually decreasing. The value of the  $p$ -criterion in this interval of the formed geo-statistical model fluctuates around 0.000–0.013.

Correlation field  $B = f(|A_D - A_p|)$  based on the results of regression analysis for reflecting horizon  $I^P$  is shown in Fig. 1, d.

Having analyzed the data in Table 4 and Fig. 1, d, we can conclude that the boundary value of the  $|A_D - A_p|$  parameter is in the range from 7 to 8 m (7.5 m is taken as the average value).

#### Justification of the boundary values of the parameter $|A_D - A_p|$ for the reflecting horizon $I^E$

Table 5 presents the results of the regression study  $A_D = f(A_p, S, D, S/D, S_{RH}, I, \gamma, L^1_C, L^1_E, D^1_C, L^2_C, L^2_E)$  with the  $|A_D - A_p|$  parameter in ascending order for the reflecting horizon  $I^E$ .

As can be seen from Table 5, the regression was performed for  $N$  from 8 to 21 structures inclusive for the reflecting horizon  $I^E$ .

The results of this regression study for reflecting horizon  $I^E$  allowed combining the obtained geo-statistical models, similar in the nature of significant parameters influence. Thus, for the reflecting horizon  $I^E$  two classes of structures were identified.

Class "1" corresponds to the first stable geo-statistical model, observed at  $N$  from 8 to 17.

Statistically significant parameters that control the model in this interval are  $A_p$  and fragmentary  $A_p$ ,  $S$ ,  $D$ ,  $S/D$ ,  $S_{RH}$ ,  $I$ ,  $\gamma$ ,  $L^1_C$ ,  $D^1_C$ ,  $L^2_C$ . The multiple correlation coefficient ( $R^2$ ) in this interval varies from 0.799 up to 1,000, gradually decreasing.

The value of the  $p$ -criterion in this interval of the formed geo-statistical model fluctuates around 0.000–0.002.

The geo-statistical model is reconstructed from the first to the second at  $N$  equal to 18.

Table 5

Results of the regression study  $A_D = f(A_p, S, D, S/D, S_{RH}, I, \gamma, L^1_C, L^1_E, D^1_C, L^2_C, L^2_E)$   
with the  $|A_D - A_p|$  parameter in ascending order by the reflecting horizon  $I^E$

| No | $A_p$ , m | $A_D$ , m | $ A_D - A_p $ , m | B, fr. of units | Coefficients for parameters, fractions of units. |          |        |        |       |        |          |         |         |         | $R^2$ , fr. of units | $p$ -cr., fr. of units | $SE$ , m |       |       |       |
|----|-----------|-----------|-------------------|-----------------|--|----------|--------|--------|-------|--------|----------|---------|---------|---------|----------------------|------------------------|----------|-------|-------|-------|
|    |           |           |                   |                 | $A_p$  | $S_{RH}$ | $I$    | $D$    | $S$   | $S/D$  | $\gamma$ | $L^1_C$ | $L^1_E$ | $D^1_C$ | $L^2_C$              | $L^2_E$                |          |       |       |       |
| 1  | 4         | 4         | 0                 |                 |  |          |        |        |       |        |          |         |         |         |                      |                        |          |       |       |       |
| 2  | 6         | 6         | 0                 |                 |  |          |        |        |       |        |          |         |         |         |                      |                        |          |       |       |       |
| 3  | 8         | 8         | 0                 |                 |  |          |        |        |       |        |          |         |         |         |                      |                        |          |       |       |       |
| 4  | 9         | 9         | 0                 |                 |  |          |        |        |       |        |          |         |         |         |                      |                        |          |       |       |       |
| 5  | 2         | 3         | 1                 |                 |  |          |        |        |       |        |          |         |         |         |                      |                        |          |       |       |       |
| 6  | 2         | 3         | 1                 |                 |  |          |        |        |       |        |          |         |         |         |                      |                        |          |       |       |       |
| 7  | 4         | 5         | 1                 |                 |  |          |        |        |       |        |          |         |         |         |                      |                        |          |       |       |       |
| 8  | 11        | 10        | 1                 | -0.491          | 0.880  | 0.272    | -0.025 |        | 0.763 |        | 0.116    |         | -4.496  |         | 1.000                | 0.001                  | 0.005    |       |       |       |
| 9  | 11        | 8         | 3                 | 2.112           | 0.733  |          |        |        |       |        |          |         |         |         | -0.087               | 0.956                  | 0.000    | 0.637 |       |       |
| 10 | 12        | 9         | 3                 | 2.246           | 0.717  |          |        |        |       |        |          |         |         |         | -0.098               | 0.958                  | 0.000    | 0.615 |       |       |
| 11 | 5         | 9         | 4                 | 2.103           | 0.517  |          |        |        |       |        |          |         |         |         | 0.084                | 0.799                  | 0.002    | 1.307 |       |       |
| 12 | 13        | 17        | 4                 | 12.920          | 0.458  | 8.689    | 0.294  | -8.126 |       | -9.656 | -0.042   |         |         |         |                      | -0.100                 | 0.988    | 0.001 | 0.699 |       |
| 13 | 7         | 2         | 5                 | 15.681          | 0.535  |          | -0.494 |        |       |        |          | -0.147  |         |         |                      | -0.315                 | 0.850    | 0.002 | 1.903 |       |
| 14 | 9         | 4         | 5                 | 16.212          | 0.525  |          | -0.523 |        |       |        |          | -0.150  |         |         |                      | -0.329                 | 0.856    | 0.001 | 1.804 |       |
| 15 | 13        | 8         | 5                 | 17.072          | 0.455  |          | -0.538 |        |       |        |          | -0.144  |         |         |                      | -0.367                 | 0.836    | 0.001 | 1.830 |       |
| 16 | 13        | 7         | 6                 | 18.466          | 0.343  |          | -0.475 |        |       |        |          | -0.158  |         |         |                      | -0.409                 | 0.818    | 0.000 | 1.836 |       |
| 17 | 14        | 7         | 7                 | 23.396          |  | 0.452    | -0.333 |        |       |        |          | -0.227  |         |         |                      | -0.578                 | 0.144    | 0.818 | 0.001 | 1.837 |
| 18 | 4         | 13        | 9                 | 12.720          |  |          | -0.238 |        |       |        |          | -0.890  |         | 35.457  |                      | 0.511                  | 0.016    | 2.883 |       |       |
| 19 | 20        | 10        | 10                | 13.357          |  |          |        |        |       |        | -0.197   |         |         |         |                      | 0.350                  | 0.008    | 3.058 |       |       |
| 20 | 17        | 4         | 13                | 13.030          |  |          |        |        |       |        | -0.184   |         |         |         |                      | 0.373                  | 0.004    | 2.988 |       |       |
| 21 | 18        | 2         | 16                | 14.384          |  |          | -0.266 |        |       |        | 0.037    |         |         |         |                      | 0.328                  | 0.073    | 3.344 |       |       |

Table 6

Comparison of structural constructions the error for reflecting horizons III,  $II^P$ ,  $II^E$ ,  $I^P$ ,  $I^E$   
based on the results of 3D CDP seismic exploration with boundary  $|A_D - A_p|$  parameter values

| Reflecting horizon | Limit value $ A_D - A_p $ , m | Accuracy of structural constructions based on the results of 3D CDP seismic exploration works, m |                            |                            |                            | The difference between the average value of structural accuracy and the boundary value $ A_D - A_p $ , m |                            |                            |                            |
|--------------------|-------------------------------|--|----------------------------|----------------------------|----------------------------|--|----------------------------|----------------------------|----------------------------|
|                    |                               | Average value (min/max)  |                            | Southern part of Perm Krai |                            | Northern part of Perm Krai   |                            | Southern part of Perm Krai |                            |
|                    |                               | Southern part of Perm Krai   | Northern part of Perm Krai | Southern part of Perm Krai | Northern part of Perm Krai | Southern part of Perm Krai   | Northern part of Perm Krai | Southern part of Perm Krai | Northern part of Perm Krai |
| III                | > 14                          | 18.9<br>(10/32.5)  | 28.9<br>(21.2/41)          |                            |                            | < 4.9  |                            |                            | < 14.9                     |
| $II^P$             | 11.5                          | 12.4<br>(6.4/16.8)   | 23.2<br>(12.9/33.9)        |                            |                            | 0.9  |                            |                            | 11.7                       |
| $II^E$             | 9.5                           | 12.1<br>(8/17.4)   | 24.2<br>(13.2/34.2)        |                            |                            | 2.6  |                            |                            | 14.7                       |
| $I^P$              | 7.5                           | 10.1<br>(6/16.5)   | 22.3<br>(9.1/35)           |                            |                            | 2.6  |                            |                            | 14.8                       |
| $I^E$              | 8                             | 9.8<br>(7/15.1)  | 15.9<br>(15.9/15.9)        |                            |                            | 1.8  |                            |                            | 7.9                        |

Class "2" corresponds to the second stable geo-statistical model, observed at  $N$  from 18 to 21.

Statistically significant parameters that control the model in this interval are  $L^1_C$  and, fragmentarily,  $D^1_C$ .

The coefficient of multiple correlation ( $R^2$ ) in this interval varies from 0.328 to 0.511, gradually decreasing. The value of the  $p$ -criterion in this interval of the formed geo-statistical model fluctuates around 0.004–0.073.

Correlation field  $B = f(|A_D - A_p|)$  based on the results of regression analysis for reflecting horizon  $I^E$  is shown in Fig. 1, e.

Having analyzed Table 5 and Fig. 1, e, we can conclude that the boundary value of the  $|A_D - A_p|$  parameter is in the range from 7 to 9 m (8 m is taken as the average).

#### Justification for the correspondence of structural maps of reflecting horizons

To justify the correspondence of structural maps of reflecting horizons III,  $II^P$ ,  $II^E$ ,  $I^P$ ,  $I^E$  summary correlation fields were constructed between each other  $k(A_p) = f(|A_D - A_p|)$  where  $k(A_p)$  is the coefficient value at  $A_p$  (Fig. 2).

To justify the correspondence of structural maps of reflecting horizons, the equations of trend lines and variation ranges in the coefficient value at  $A_p$  were analyzed for each reflecting horizon:

- the trend line equation for reflecting horizon III is  $k(A_p) = 1.7352 - 0.0997 * (|A_D - A_p|)$ , with a range of variation in  $k(A_p)$  from 0.505 to 1.818;

- the trend line equation for reflecting horizon  $II^P$  is  $k(A_p) = 1.1194 - 0.0129 * (|A_D - A_p|)$ , with a range of variation in  $k(A_p)$  from 0.723 to 1.213;

- the trend line equation for reflecting horizon  $II^E$  is  $k(A_p) = 1.0822 - 0.0136 * (|A_D - A_p|)$ , with a range of variation in  $k(A_p)$  from 0.692 to 1.156;

- the trend line equation for reflecting horizon  $I^P$  is  $k(A_p) = 0.7272 - 0.0271 * (|A_D - A_p|)$ , with a range of variation in  $k(A_p)$  from 0.463 to 0.786;

- the trend line equation for reflecting horizon  $I^E$  is  $k(A_p) = 0.9934 - 0.1049 * (|A_D - A_p|)$ , with a range of variation in  $k(A_p)$  from 0.343 to 0.880;

Thus, for the reflecting horizons  $II^P$  and  $II^E$ , the trend lines  $k(A_p)$  are practically parallel to each other, and  $k(A_p)$  takes values in the general range from 0.692 to 1.213, whereas for the reflecting horizons  $I^P$  and  $I^E$ , a clearly non-zero angle is observed between the trend lines  $k(A_p)$ , but  $k(A_p)$  also takes values in the general range from 0.343 to 0.880 (it is necessary to take into account the unequal size of samples for different reflecting horizons).

Based on the provided data, it can be concluded that the structural plans for the pairs of reflecting horizons  $II^P - II^E$  and  $I^P - I^E$  correspond to each other, while their plans do not correspond to the structural plan for reflecting horizon III. This confirms the geological structure concept of the southern part of the Perm Krai.

#### Comparison of the obtained boundary values with the results of calculating the accuracy of structural constructions performed within the framework of the 3D CDP seismic exploration reports

To compare the previously obtained boundary values of  $|A_D - A_p|$  parameter with the accuracy of the structural constructions reflecting horizons III,  $II^P$ ,  $II^E$ ,  $I^P$ ,  $I^E$  based on

the results of 3D CDP seismic surveys in the southern part of the Perm Krai, 27 reports on seismic exploration works were analyzed from 2007 to 2019 to assess the accuracy of structural constructions for reflecting horizons [53, 54].

In all the studied reports, the structural constructions accuracy was assessed according to the requirements set out in the document "Guidelines for the Evaluation of the Quality of Structural Constructions and the Reliability of Identified Objects Based on CDP Seismic Reflection Method, 1984" [55].

As can be seen from Table 6, the structural constructions, as well as the previously calculated boundary values of the  $|A_D - A_p|$  parameter, have a minimum error at the overlying horizons and a maximum error at the underlying horizons.

For comparison, Table 6 shows the error values of structural constructions for the northern part of the Perm Krai (according to data from nine reports on the results of 3D seismic exploration works carried out at the same time).

The southern part of the Perm Krai is characterized by little difference between the average value of structural constructions accuracy calculated by the results of 3D seismic exploration work and the boundary value  $|A_D - A_p|$  (for reflecting horizon III – no more than 4.9 m, for II<sup>P</sup> – 0.9 m, for II<sup>E</sup> – 2.6 m, for I<sup>P</sup> – 2.6 m, for I<sup>E</sup> – 1.8 m), while for the northern part of the Perm Krai it is characterized by a large one (for reflecting horizon III – no more than 14.9 m, for II<sup>P</sup> – 11.7 m, for II<sup>E</sup> – 14.7 m, for I<sup>P</sup> – 14.8 m, for I<sup>E</sup> – 7.9 m).

The small difference between the average value of the structural constructions accuracy calculated by the results of 3D CDP seismic surveys for the southern part of the Perm Krai and the boundary value  $|A_D - A_p|$  obtained in this study allows us to conclude that the southern part of the Perm Krai is more thoroughly studied compared to its northern part. It also confirms the applicability of the geo-statistical methods used, which support the conformity of structural plans of the main reflecting horizons, mainly for the southern part of the Perm Krai.

## Conclusion

This study examined one of the options for developing a geo-statistical approach to assessing the accuracy of structural constructions of the studied sample based on the analysis of structure amplitudes dependencies according to

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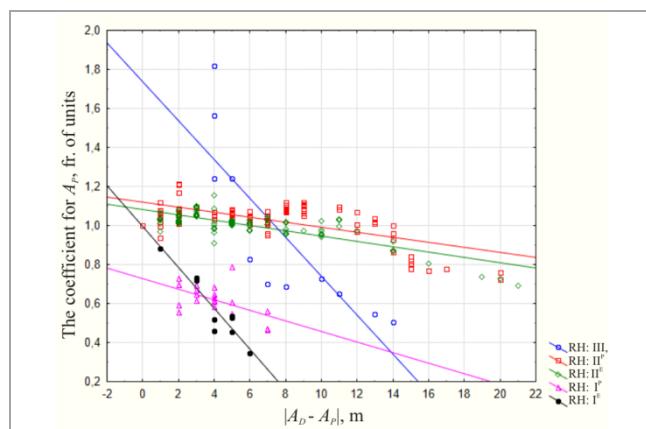


Fig. 2. Combined Correlation Field  $k(A_p) = f(|A_D - A_p|)$  according to the results of regression analysis

prospecting and appraisal drilling data on various geo-morphological parameters. For each model, the nature and degree of significant parameters influence on the confirmability of the amplitude by drilling were determined and described.

This approach allowed us to draw conclusions about the degree of territory study under consideration. Based on the results obtained, it was concluded that the structural plans of reflecting horizons in the southern part of the Perm Krai correspond to each other. Thus, in the southern part of the Perm Krai can be observed a correspondence of structural plans separately for pairs of reflecting horizons IIP – IIE and IP – IE and a mismatch of their plans with the structural plan of reflecting horizon III, which confirms the geological structure concept of the studied territory.

The obtained boundary values of discrepancies were compared with the errors of structural constructions assessed by the results of 3D CDP seismic exploration in the Perm Krai. Based on this, conclusions were drawn that the southern part of the Perm Krai is more thoroughly studied compared to its northern part.

This geo-statistical approach can be used to clarify the risks associated with the problem of geo-morphological characteristics unconfirmability of structures by deep drilling.

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