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Determination of the Optimal Injection Ratio of Fluids in Water-Gas Influence

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Определение оптимального соотношения закачки флюидов при водогазовом воздействии

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Water-gas stimulation, water-gas mixture, gas-oil contact, horizontal well, gas factor, associated petroleum gas, reservoir pressure maintenance, near-wellbore zone, enhanced oil recovery, oil recovery coefficient, hydrocarbons, compositional model, pilot industrial operations, modeling, correlation.

Hard-to-recover reserves are increasing in size every year, and the classical development of fields with such reserves is not so effective, therefore the application of enhanced oil recovery methods is relevant. Such method of enhanced oil recovery as water-gas stimulation will be presented in this paper.

There are two types of water-gas simulation: alternating water and gas injection and simultaneous injection. Alternating water and gas injection is focused in this work. The process involves the sequential injection of gas followed by water. This method is widely implemented, and experience in conducting such operations has already been accumulated. The goal was to identify scenarios that could cover the realistically possible conditions for the application of water-gas stimulation and to find the optimally effective ratio of water and gas injection. The parameters for ranking included reservoir permeability, reservoir compartmentalization, the development system with various well designs and spacing between wells, as well as various volumes of injected agents (water, gas).

Multivariate calculations were carried out on a sectoral hydrodynamic model (E300). Since experiments on miscibility conditions were not conducted, it was assumed that oil displacement during water-gas influence occurred without gas mixing with oil.

Based on the processing of the entire dataset (more than 10,000 calculations), a database of development systems with various input geological and physical characteristics was formed and dependencies for cumulative oil production at different volumes of water and gas injection were obtained.

The effect of water-gas stimulation is noticeable with reservoir permeability greater than 20 mD. The effective water and gas injection ratio should ensure that the liquid withdrawal compensation is above 100%, both for water and gas injection.

Ключевые слова:

водогазовое воздействие, водогазовая смесь, газонефтяной контакт, горизонтальная скважина, газовый фактор, попутный нефтяной газ, поддержание пластового давления, призабойная зона пласта, повышение нефтеотдачи пласта, коэффициент извлечения нефти, углеводород, композиционная модель, опытно-промышленные работы, моделирование, корреляция.

Трудноизвлекаемые запасы растут с каждым годом, и классическая разработка месторождений с такими запасами не так эффективна, поэтому применение методов увеличения нефтеотдачи актуально. В работе будет представлен метод увеличения нефтеотдачи как водогазовое воздействие.

Классифицируют два вида водогазового воздействия: попеременная закачка воды и газа и совместная. В исследовании рассматривается попеременная закачка воды и газа. Сам процесс представляет собой порционную закачку сначала газа, затем воды.

Данный метод обширно внедряется и уже накоплен опыт проведения таких мероприятий, целью было сформировать такие сценарии, чтобы в наибольшей степени охватить реально возможные условия применения водогазового воздействия и найти при этом оптимальное соотношение закачки воды и газа. Под параметры ранжирования были взяты проницаемость коллектора, расщлененность пласта, система разработки с различными конструкциями скважин и расположением между скважинами, а также различные объемы закачиваемого агента (вода, газ).

Многовариантные расчеты проводились на секторной гидродинамической модели (E300). Так как опыты на условие смесимости не проводились, считалось, что вытеснение нефти при водогазовом воздействии происходит без смешения газа и нефти.

По результатам обработки всего массива данных (более 10 000 расчетов) была сформирована база систем разработок с различными входными геолого-физическими характеристиками, где получены зависимости накопленной добычи нефти при различных объемах закачки воды и газа.

Эффект применения водогазового воздействия заметен при проницаемости коллектора более 20 мД. Эффективное соотношение закачки воды и газа – это компенсация отборов жидкости, которая должна быть выше 100 % как при закачке воды, так и закачке газа.

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Introduction

The relevance of this topic is due to the growing share of hard-to-recover reserves, which makes water-gas stimulation of formations (WGS) a promising tool for achieving economic benefits through enhanced oil recovery.

The technology of water-gas stimulation is becoming attractive for implementation, and the number of measures taken is growing. The greatest application of this technology was found at the Samotlor field. The effect obtained from this measure is unique: the amount of additional oil produced at this field was greater than oil production at other fields [1–8].

This type of geological and technical intervention - water-gas stimulation - was carried out at such fields as Samotlor, Bitkovskoye, Ileshevskoye, Alekseevskoye and had positive results [9–18].

At the Samotlorskoye field WGI made it possible to increase oil production and reduce water cut at the pilot development area. As a result of these measures the oil recovery factor was increased by more than 5 %.

At the Bitkovskoye field this technology increased the oil recovery factor by 16 %. This result was achieved by increasing reservoir pressure (the decline trend changed), thereby increasing the oil flow rate and stabilising the gas factor. Additional production from water-gas stimulation amounted to 750 thousand tonnes of oil.

The application of WGI at the Ileshevskoye field (1999) gave a positive result. The effect of the measures was recorded in the form of increased oil production, reduced water and associated gas production.

At the Alekseevskoye field WGI has been carried out since 2005. By mixing produced water and associated gas the mixture was injected into the well. The effect of this measure made it possible to increase the oil recovery factor by 40 % (from 0.170 fractions of unit to 0.240 fractions of unit).

The effect of this technology was also obtained at other fields. For example, at the Vakhovskoye field about 5 thousand tonnes of additional produced oil were obtained due to water-gas simulation.

How much to pump? What is the volume of gas and water injection? And under what geological conditions water-gas injection will show itself better? And what is the injection mode? These questions will be answered in the course of this work.

Criteria and Approaches

Water-gas stimulation is the economically expensive activity. It requires specialists with extensive experience and equipment to ensure reliability and safety of such hydrodynamic modelling (HDM).

To select the conditions for performing WGS the analysis of A.I. Vashurkin and M.S. Svishchev study was used. The criteria are presented in Fig. 1.

The generated variants were calculated on a hydrodynamic model. The model of E300 type [19–37] satisfies all the conditions for taking into account the movement of three phases (Fig. 2). With its help it is possible to consider how a hydrocarbon fluid displaces gas of different component composition.

Obtaining plausible calculations is achieved by using a sector model which satisfies the applicability criteria for conducting WGS (Table).

Different degrees of uncertainty are found in all areas. Hydrocarbon extraction is no exception, and uncertainties can be found in both surface and subsurface infrastructure (Fig. 3).

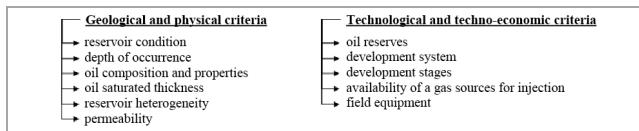


Fig. 1. WGS site selection criteria

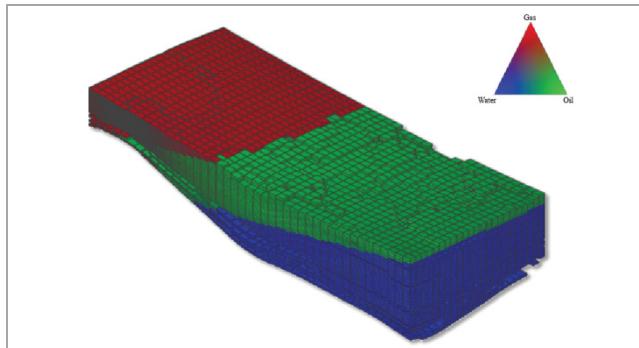


Fig. 2. Sectoral WGS for carrying out multivariate calculations

Parameters of the sector hydrodynamic model

Parameter	Value
Initial oil saturation, %	85
Initial water saturation, %	15
$P_{in,res}$, MPa	13.1
P_{sat} , MPa	13.1
$K_{porosity}$, %	15
$K_{compressibility}$, Mpa^{-1}	10^{-4}
$K_{permeability}$, mD	355
Gas content, m^3/t	75

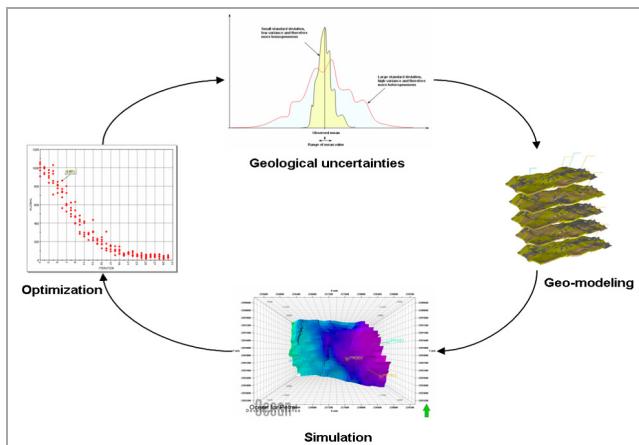


Fig. 3. Methodology for systematic uncertainties analysis

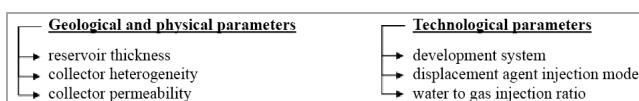


Fig. 4. Parameters for variations

5-point	7-point	9-point	inline
300x300 metres;	300x300 metres;	300x300 metres;	TC500 300 metres between the rows;
500x500 metres;	500x500 metres;	500x500 metres;	TC500 500 metres between the rows;
TC500 metres;	TC500 metres;	TC500 300x300 metres;	TC700 300 metres between the rows;
TC700 metres;	TC700 metres;	TC500 500x500 metres;	TC700 300 metres between the rows;
		TC700 300x300 metres;	
		TC700 500x500 metres;	

Injection modes

- water injection only;
- gas injection only;
- 1 month water injection / 1 month of gas injection;
- 1.5 months water injection/1.5 months gas injection;
- 1 month water injection/1.5 months gas injection;
- 1.5 month water injection/1 months gas injection

Fig. 5. List of well grids and injection modes

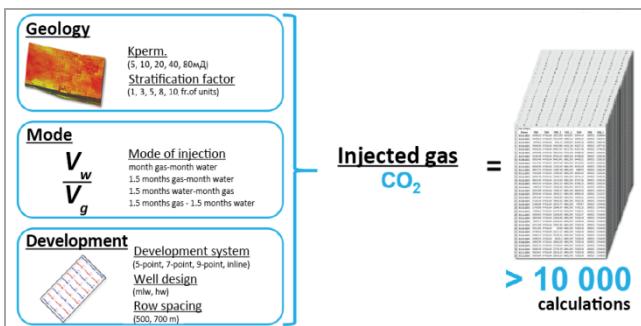


Fig. 6. Scope of data for the study

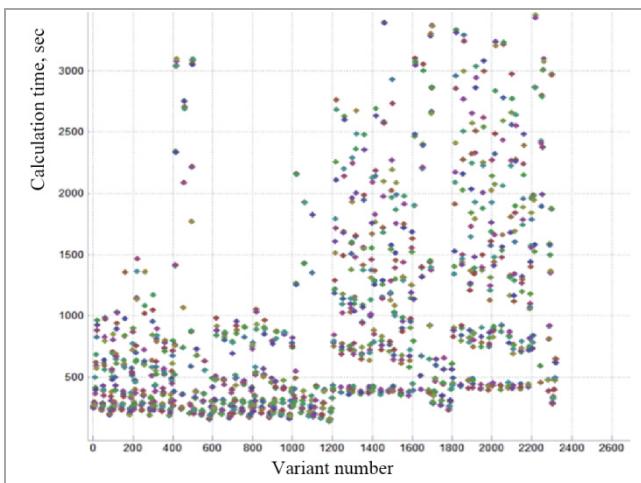


Fig. 7. Fragment of dependency of calculation time duration from variant number

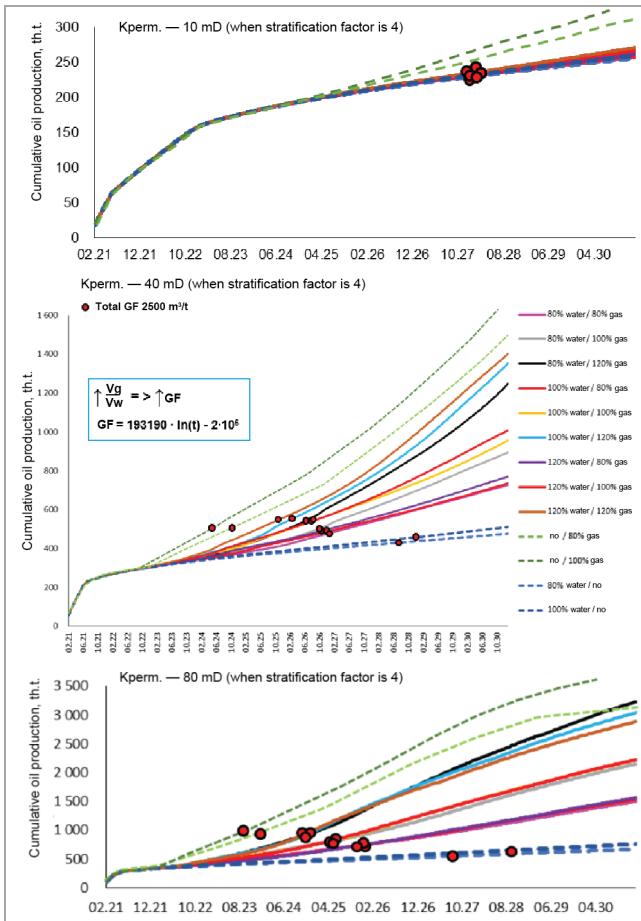


Fig. 8. Distribution of cumulative oil production depending on the ratio of injection volumes of agents (water and gas)

For risk mitigation the solution which covers most of the possible combinations of the criteria enumeration is used. The main geological-physical and technological parameters [38–45], affecting the conditions of applicability of the technology, will be varied in the work (Fig. 4).

The variation of parameters using arithmetic was set in a hydrodynamic simulator. To change the thickness of the formation and pore volume, the change in active cells due to the introduction of a non-reservoir was used. Reservoir heterogeneity and permeability were selected by the analysis of the actual experience of the technology (values for reservoir heterogeneity – 1, 4, 8, for permeability – 5, 10, 20, 40, 80 мД).

The approach to field development is individual, so creating scenarios with technological parameters was time-consuming.

Different well designs, their location in relation to each other and so on do not give a clear understanding of the impact of gas and water injection. Therefore, in order to cover a large volume, the most common models of well spacing (18 variants) were formed to make calculations on hydrodynamic simulator. Six injection modes were also considered (Fig. 5).

The total generated data set is more than 10.000 calculations (Fig. 6).

Each calculation took different time: from 3 min to 1 h. The duration of the calculation depended on the number and design of wells and injection mode (Fig. 7).

Results

The results were analysed on the example of a five-point development system with 500 m long horizontal wells under different water and gas injection modes, permeability of the reservoir and its compartmentalization. To assess the effect of water-gas influence, the indicator of cumulative oil production over time was taken. The gas factor (GF > 2500 м³/t) is the criterion affecting the success of the variant. Due to high GF values, there are complications in the operation of downhole pumping equipment, as well as infrastructure limitations.

The results of the calculations are presented in Fig. 8.

Discussion

The analyses of all varying parameters show that at reservoir permeability less than 10 mD the effect of WGS is insignificant and not very sensitive to different variations of gas and water injection modes, while the displacing agent of gas injection is more effective, both at 80 % and 100 % compensation of withdrawals. This is associated with the fact that gas (CO_2) has greater mobility. When mixed with the oil phase it reduces its viscosity and capillary forces holding back residual oil.

However, with increasing permeability (> 20 mD) the gas factor becomes a limiting factor in the efficiency of the measure. At the same time the gas factor correlates with the injected volume of gas and water. The more gas is injected into the reservoir the earlier the gas factor limit values are reached. Further efficiency of the WGS technology depends on the economic component.

Conclusion

The effect of water-gas stimulation is noticeable at permeability of the reservoir more than 20 mD. The effective ratio of water injection to gas injection is the compensation of fluid withdrawals and should be higher than 100 % for both water and gas injection.

Based on the results of processing the entire data set (more than 10,000 calculations) it has been formed a database of development systems with different input geological and physical characteristics. According to this database applicability criteria at which the water-gas impact is successful have been determined.

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